

A Calibration Technique for Very Low Current and Compact Tunable Neuromorphic Cells: Application to 5-bit 20-nA DACs

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Abstract—Low current applications, like neuromorphic circuits, where operating currents can be as low as a few nanoamperes or less, suffer from huge transistor mismatches, resulting in around or less than 1-bit precisions. Recently, a neuromorphic programmable-kernel 2-D convolution chip has been reported where each pixel included two compact calibrated digital-to-analog converters (DACs) of 5-bit resolution, for currents down to picoamperes. Those DACs were based on MOS ladder structures, which although compact require $3N + 1$ unit transistors (N is the number of calibration bits). Here, we present a new calibration approach not based on ladders, but on individually calibratable current sources made with MOS transistors of digitally adjustable length, which require only N -sized transistors. The scheme includes a translinear circuit-based tuning scheme, which allows us to expand the operating range of the calibrated circuits with graceful precision degradation, over four decades of operating currents. Experimental results are provided for 5-bit resolution DACs operating at 20 nA using two different translinear tuning schemes. Maximum measured precision is 5.05 and 7.15 b, respectively, for the two DAC schemes.

Index Terms—Analog, calibration, mismatch, subthreshold.

I. INTRODUCTION

OVER THE LAST 20 years, a vast amount of neuromorphic VLSI systems have been reported which usually consist of large arrays of special processing pixels. Since pixel size has to be of reduced size and power consumption, analog design techniques are used with transistors of small size operating with nanoamperes or less. This yields necessarily high mismatch. Although reported neuromorphic VLSI systems have revealed interesting, powerful, and fast information sensing and processing capabilities, they still have not evolved clearly to specific marketable products. One of the main reasons for this is the unavoidable excessive mismatch. For example, a $2.5 \mu\text{m} \times 1.5 \mu\text{m}$ nMOS at 20 nA has a mismatch of $\sigma \approx 8\%$ (see [4, Fig. 3]). Defining LSB as 6σ , this yields a precision of $\log_2 6\sigma = 1$ b or, to design a 5-bit current source at 20 nA, one needs a $160 \mu\text{m} \times 10 \mu\text{m}$ nMOS [4].

To keep mismatch low without increasing transistor sizes nor operating currents, the only known solution is calibration.

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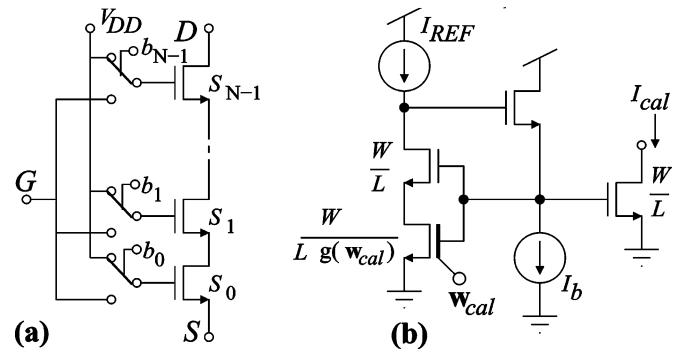


Fig. 1. (a) Schematics of proposed digitally controlled length MOS transistor. (b) Application to a calibration current source.

Some researchers have reported calibration techniques based on floating-gate MOS transistors [5], [6] in standard CMOS processes. However, these techniques require large area and special know-how. Recently, some neuromorphic systems with in-pixel RAM-based calibration techniques have been reported [1]–[3], [7], which exploit the use of compact current digital-to-analog converters (DACs) made with calibratable MOS ladder structures [8]. The drawback of this approach is that it uses a one-point calibration principle, which limits the final precision to 3 bits for nano amp currents and practical transistor sizes. In this paper, we present another principle with which we have achieved up to 7.15 b.

II. MOS WITH DIGITALLY ADJUSTABLE LENGTH

Previously reported in-pixel RAM-based calibration circuits [1], [2] were based on the use of MOS ladder structures [8].

With these structures, we obtained in the past [8] 4.4 bits at $2 \mu\text{A}$ with $16.5 \mu\text{m} \times 5 \mu\text{m}$ nMOS transistors (total active area = $400 \mu\text{m}^2$), for the same $0.35\text{-}\mu\text{m}$ CMOS technology we are using in the present work.

In this paper, we present a new approach to digitally adjust the equivalent size of a MOS transistor using a more compact circuitry. Fig. 1(a) shows the schematics of the new digi-MOS (digitally controlled-length MOS). There are N transistor segments between terminals D and S . Each segment is either enabled by connecting its gate to terminal G or disabled by connecting its gate to V_{DD} (for noise-sensitive applications, this node should be a low-noise V_{DD}). Transistor sizes can be, for example, $S_{N-1} = W/L$, $S_{N-2} = 2W/L \dots$, and $S_0 = (2^{N-1})W/L$. This can be implemented physically by using unit transistors of size W/L

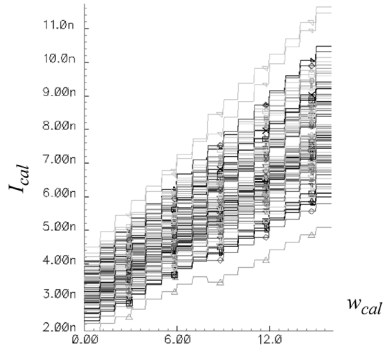


Fig. 2. Monte Carlo simulation (with 100 iterations) of the circuit in Fig. 1(b), using a 4-bit digitally controlled length MOS.

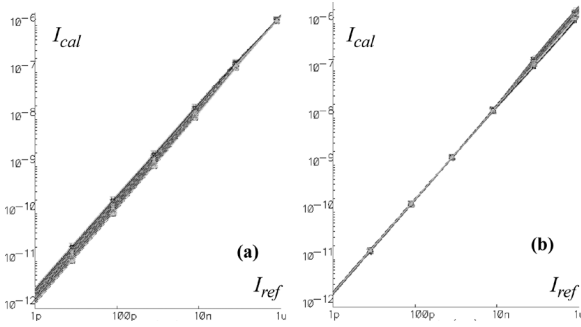


Fig. 3. Monte Carlo simulation results for the circuit in Fig. 1(b) when sweeping I_{REF} . (a) Before calibration with $w = 15$ for all Monte Carlo iterations. (b) After calibration with optimum w for each iteration.

(one for S_{N-1} , two in parallel for $S_{N-2}, \dots, 2^{N-1}$ in parallel for S_0). This way, each segment would be equivalent to a transistor of size $S_i = W / (L/2^{N-i-1})$. The operation of this circuit is region-independent and can be analyzed by simple transistor series/parallel association [10]. Consequently, the digitally adjustable transistor in Fig. 1(a) would be equivalent to one of width W and digitally adjustable length $L_{eq} = L \times g(w_{cal})$ where $w_{cal} = b_{N-1} \dots b_1 b_0$ and $g(w_{cal}) = \sum_{i=0}^{N-1} b_i 2^{1+i-N}$. This transistor can be used as part of a current mirror,¹ as shown in Fig. 1(b), to provide a calibration current $I_{cal} = I_{REF} \times (g(w_{cal}) + 1)$. Fig. 2 shows the simulated stairs of I_{cal} as a function of w_{cal} (using a 4-bit digitally controlled-length MOS) with $I_{REF} = 3$ nA, using unit MOS sizes of $1 \mu\text{m}/4 \mu\text{m}$, and models for a $0.35\text{-}\mu\text{m}$ standard CMOS process. Fig. 3(a) shows I_{cal} as function of I_{REF} before calibration, with $w_{cal} = 15$ for each of the 100 simulated Monte Carlo iterations. The mismatch at $I_{REF} = 3$ nA is $\Delta I_{cal}/I_{REF} = 110\%$ and at $I_{REF} = 1$ pA is 130% . Using the results in Fig. 2 (for $I_{REF} = 3$ nA), one can compute for each Monte Carlo iteration the optimum value of w_{cal} for minimum spread at I_{cal} . Once setting this optimum set of values for w_{cal} , the resulting I_{cal} as function of I_{REF} is shown in Fig. 3(b). Now, the mismatch at $I_{REF} = 3$ nA has been reduced to 4% (4.6 b).

From a practical point of view, it is not efficient to follow the previous unit transistor-based sizing strategy, because the

¹Here we use a subpico-ampere current mirror topology [11], since we want to use eventually I_{REF} values down to the *pico ampere* range [2].

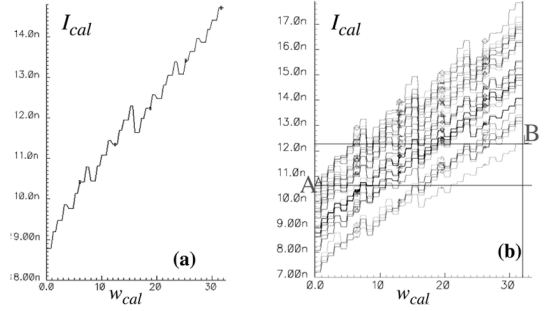


Fig. 4. Example simulation of a 5-bit digitally controlled length MOS with one transistor per segment and intentional down-steps. (a) Nominal mismatch-less simulation. (b) Monte Carlo simulation with 100 iterations.

number of unit transistors doubles with number of bits. In practice, it is more efficient to use one single transistor for each segment (bit) and adjust its size to have a similar effect. Furthermore, from a statistical point of view, we are not looking for nice uniform staircases, but for a (random) coverage. The maximum step heights will limit the final calibration capability. Therefore, it is important to minimize this maximum possible step height. To do this, we design the nominal stair case with some intentional “down-steps,” so that when mismatch introduces random variations the extra redundancy (coverage) compensates for eventual large up-steps. Fig. 4, for example, shows Monte Carlo simulation results of a 5-bit structure that uses one single transistor per segment and has intentional down-steps. Simulated and fabricated transistor sizes are $\{2/3, 2/1.8, 2/1.8, 2/1, 2/0.7\}$. Consequently, total active area is now $16.6 \mu\text{m}^2$.

III. TRANSLINEAR CIRCUITS FOR TUNING

The calibration technique shown in Fig. 1 requires to recalibrate all circuits when there is a global change in the operating current I_{REF} . In practice, it is desirable to allow a change in the operating current I_{REF} without requiring recalibration. Note that all transistors introduce mismatching and calibration compensates for the combination of all mismatches of all transistors. The mismatch introduced by each transistor is dependent on its operation current and bias conditions. To have calibration less sensitive to bias conditions one should use topologies that change bias conditions for as few transistors as possible. To achieve this, we use tunable translinear circuits, which will allow us to keep fixed bias currents for some transistors, including the digitally controlled-length ones. This is shown in Fig. 5. The circuitry comprised by broken lines is replicated once per pixel, but the rest is implemented only once at the periphery. Transistors M_1 to M_4 form a translinear loop, thus $I_{oi} = I_1 I_2 / I_{i3}$. Local current I_{i3} is mirrored from the peripheral global current I_3 , through a current mirror with a local digitally-controlled-length MOS. To achieve a factor-2 calibration range, we include two transistors in series for this current mirror output. One of fixed size $W/2L$ and the other calibratable. Consequently, $I_{i3} = I_3 / (2 + g(w_{cal_i}))$ and $I_{oi} = (I_1 I_2 / I_3) \times (2 + g(w_{cal_i}))$. With this circuit, one can maintain (after calibration) constant currents I_3 (and I_{i3}) and I_1 , while tuning I_2 globally to scale up or down all local currents I_{oi} .

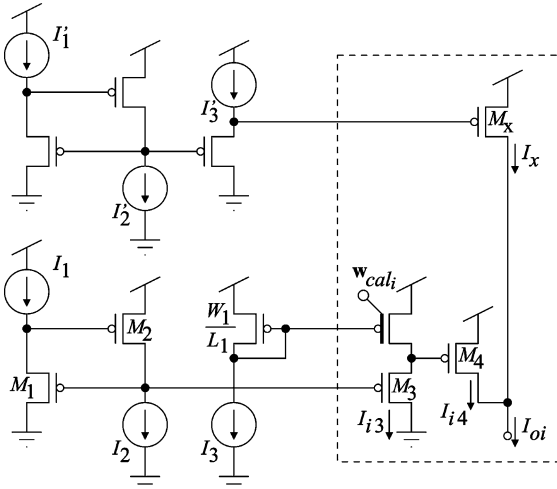
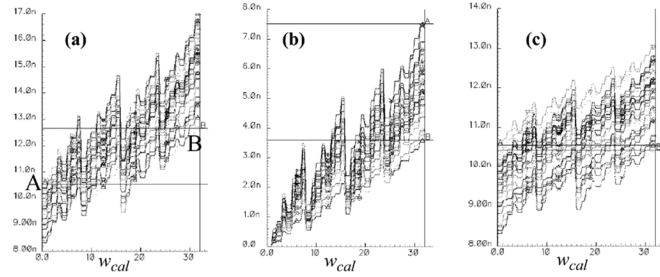
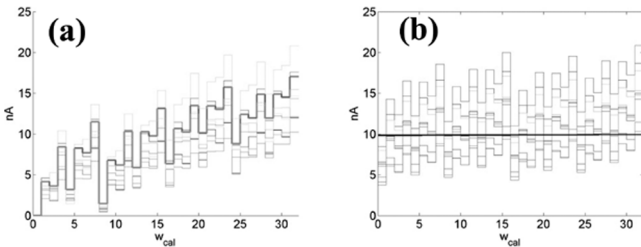


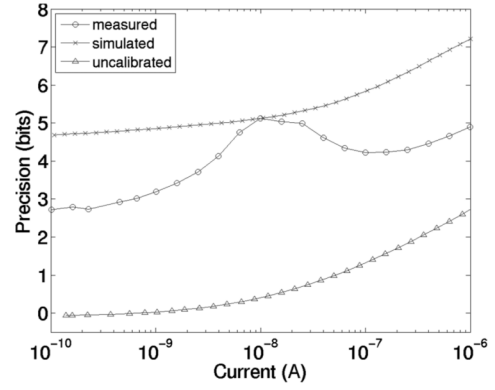
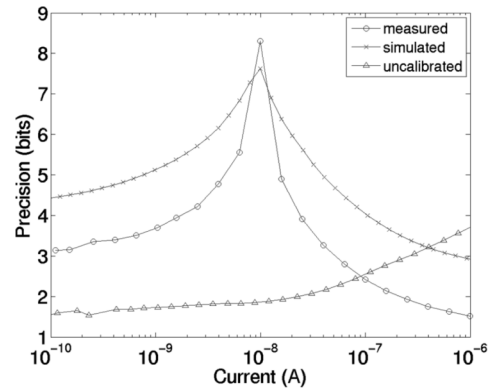
Fig. 8. Second strategy for optimizing calibration range.

Fig. 9. Simulation results for second strategy. (a) For all bias current equal to 10 nA. (b) Details of the bottom calibratable subcircuit I_{i4} . (c) Results for turning bias currents I_i down to 4.5 nA.Fig. 10. Experimentally measured output currents for the circuit in Fig. 7: (a) for $w_{adj} = 0$ and (b) for optimum w_{adj} . The horizontal line in (b) is the target value, which is cut/touched by all ten traces.

Each of the second ten DACs uses five replicas of the circuit in Fig. 8. Again, for each of the ten DACs, the circuitry is replicated five times (one per bit), and the peripheral circuitry (outside broken lines in Fig. 8) is shared, per bit, by all ten DACs.

The area of the circuit layout inside broken lines is $18 \times 14 \mu\text{m}^2$ for Fig. 6 and $17 \times 14 \mu\text{m}^2$ for Fig. 8, excluding latches.

Fig. 10(a) shows the experimentally measured output currents for ten replicas of the circuit in Fig. 6, when setting $w_{adj} = 0$. Peripheral bias currents were made equal to $I_1 = I_2 = I_3 = 10$ nA, and all calibration words w_{cali} ($i = 1, \dots, 10$) were swept simultaneously from 0 to 31. After repeating this measurement for all possible w_{adj} values, the optimum value for w_{adj} corresponds to the situation where the top left value is closest to the bottom right one. This case is shown in Fig. 10(b). At this point, we can obtain the ten optimum calibration words w_{cali} that render the minimum variation. The maximum output current spread obtained under

Fig. 11. Measured precision of calibratable and tunable current source with the approach of Fig. 6. Trace with circles: measured precision after calibration (with optimum w_{cali} for each of the ten current sources). Current sources were calibrated at 10 nA. Trace with triangles: measured precision before calibration ($w_{cali} = 0$ for all current sources). Trace with crosses: precision after calibration, obtained through simulations.Fig. 12. Measured precision of calibratable and tunable current source with the approach of Fig. 8. Trace with circles: measured precision after calibration. Current sources were calibrated at 10 nA. Trace with triangles: measured precision before calibration ($w_{cali} = 0$ for all current sources). Trace with crosses: precision after calibration, obtained through simulations.

these circumstances is $|\Delta I_{oi}|_{\max} = 0.57$ nA, which corresponds to 5.7%, at a nominal current of $I_b = 10$ nA. If this were the current source controlled by the most significant bit of a current DAC (with 20-nA maximum range), it would limit the DAC precision to $-\ln(|\Delta I_{oi}|_{\max}/2I_b) / \ln 2 = 5.13$ b. To verify how calibration degrades when changing bias conditions, we swept I_2 in Fig. 6 between 100 pA and 1 μ A. The maximum current spread among all ten calibrated current sources is shown in the trace with circles in Fig. 11. The trace with triangles are measurements obtained before calibration ($w_{cali} = 0$, for all i). We can see that the ten samples maintain a precision of 4 bits for currents above 3 nA. The horizontal axis is the average of I_{oi} among all ten samples. We also show in Fig. 11 the resulting precision after calibration obtained through simulations, shown with crosses. Note that it is over optimistic, except for the point at which calibration was done (10 nA). The reason is that usually circuit simulators do not model mismatch of slope factor (or gamma). Since the new length-controlled digi-MOS [Fig. 1(a)] is sensitive to body-effect, such mismatch affects performance, although it is not detected by most simulators.

In a similar way, Fig. 12 shows the measured precision before and after calibration of ten calibratable and tunable current

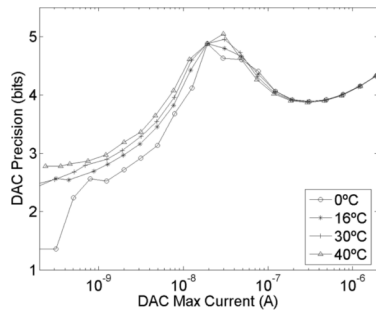


Fig. 13. Measured precision for the ten 5-bit DAC samples that use the first tuning strategy of Fig. 7. DACs were calibrated with MSB at 10 nA and at 16 °C. After calibration, precision is characterized sweeping operating current for different temperatures.

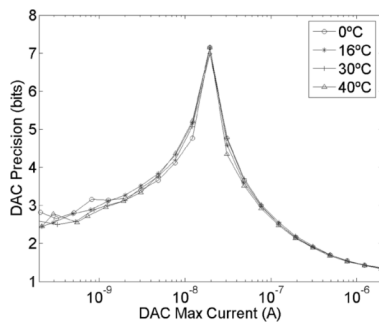


Fig. 14. Measured precision for the ten 5-bit DAC samples that use the second tuning strategy of Fig. 8. DACs were calibrated with MSB at 10 nA and at 16 °C. After calibration, precision is characterized sweeping operating current for different temperatures.

sources that follow the approach depicted in Fig. 8. Note that now the mismatch before calibration is less than that in Fig. 11. This is because now the area used by digitally controlled-length transistor M_b in Fig. 6 is available for transistor M_x in Fig. 8, which can be made larger. With the structure of Fig. 8, we obtain a much better precision at the calibration point (8.30 bits at 10 nA), but degrades rapidly, specially for high currents. The precision after calibration obtained by simulation is slightly pessimistic at the calibration point (7.63 bits at 10 nA), but it degrades optimistically as operating current departs from the calibration point (again because mismatch in slope factor (γ) is not modeled).

Figs. 11 and 12 show the matching precision among ten current sources calibrated at 10 nA. Now we use five of these sources, calibrated at $\{10, 5, 2.5, 1.25, 0.625\}$ nA, to build a 5-bit current DAC. The matching precision obtained among the ten fabricated DACs is shown in Fig. 13 (for the tuning scheme of Fig. 6) and in Fig. 14 (for the tuning scheme of Fig. 8). The DACs were calibrated at 16 °C, and the figures also illustrate the DACs behavior when temperature is changed between 0 °C and

40 °C. We can see that the effect of temperature is not severe for the lower current range, while for higher currents the DACs are almost insensitive to temperature variations.

VI. CONCLUSION

A new compact calibration scheme for current sources is presented. The approach is illustrated for current sources operating in the nano ampere range. Two tuning schemes are proposed for sweeping the operating range over four decades. The first one achieves less precision at the calibration point but it degrades more gracefully as the operating current is increased (it shows over 4-bit precision for currents larger than 10 nA). The second one achieves higher precision at the calibration point but precision degrades more as current increases (4 bits is achieved only for currents between 8–40 nA). Test prototypes have been fabricated and extensively tested and characterized. As an example application, current DACs of 5-bit resolution and 20-nA range have been fabricated and characterized.

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